Heat Conduction Equation in a Long Cylinder



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Taking the limit as $\Delta r \rightarrow 0$ and $\Delta t \rightarrow 0$ yields

$$\frac{1}{A}\frac{\partial}{\partial r}\left(kA\frac{\partial T}{\partial r}\right) + \dot{e}_{gen} = \rho c \frac{\partial T}{\partial t}$$
$$\lim_{\Delta r \to 0} \frac{\dot{Q}_{r+\Delta r} - \dot{Q}_r}{\Delta r} = \frac{\partial \dot{Q}}{\partial r} = \frac{\partial}{\partial r}\left(-kA\frac{\partial T}{\partial r}\right)$$



FIGURE 2–14

One-dimensional heat conduction through a volume element in a long cylinder.

Variable conductivity:

$$\frac{1}{r}\frac{\partial}{\partial r}\left(rk\frac{\partial T}{\partial r}\right) + \dot{e}_{\rm gen} = \rho c \frac{\partial T}{\partial t}$$

Constant conductivity:

$$\frac{1}{r}\frac{\partial}{\partial r}\left(r\frac{\partial T}{\partial r}\right) + \frac{\dot{e}_{\text{gen}}}{k} = \frac{1}{\alpha}\frac{\partial T}{\partial t}$$

$$\alpha = \kappa / \rho c$$

thermal diffusivity

1.

- (1) Steady-state: $(\partial/\partial t = 0)$
- (2) *Transient, no heat generation:* $(\dot{e}_{gen} = 0)$
- (3) *Steady-state, no heat generation:* $(\partial/\partial t = 0 \text{ and } \dot{e}_{gen} = 0)$

 $\frac{1}{r}\frac{d}{dr}\left(r\frac{dT}{dr}\right) + \frac{\dot{e}_{gen}}{k} = 0$ $\frac{1}{r}\frac{\partial}{\partial r}\left(r\frac{\partial T}{\partial r}\right) = \frac{1}{\alpha}\frac{\partial T}{\partial t}$ $\frac{d}{dr}\left(r\frac{dT}{dr}\right) = 0$

Heat Conduction Equation in a Sphere

Variable conductivity:

$$\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \, k \frac{\partial T}{\partial r} \right) + \dot{e}_{\rm gen} = \rho c \, \frac{\partial T}{\partial t}$$

Constant conductivity:

$$\frac{1}{r^2}\frac{\partial}{\partial r}\left(r^2\frac{\partial T}{\partial r}\right) + \frac{\dot{e}_{\text{gen}}}{k} = \frac{1}{\alpha}\frac{\partial T}{\partial t}$$

- (1) *Steady-state:* $\left(\frac{\partial}{\partial t} = 0\right)$
- (2) Transient, no heat generation: $(\dot{e}_{gen}=0)$

(3) Steady-state,
no heat generation:
$$(\partial/\partial t = 0 \text{ and } \dot{e}_{gen} = 0)$$



FIGURE 2-16

One-dimensional heat conduction through a volume element in a sphere.

$$\frac{1}{r^2}\frac{d}{dr}\left(r^2\frac{dT}{dr}\right) + \frac{\dot{e}_{\text{gen}}}{k} = 0$$

$$\frac{1}{r^2}\frac{\partial}{\partial r}\left(r^2\frac{\partial T}{\partial r}\right) = \frac{1}{\alpha}\frac{\partial T}{\partial t}$$

$$\frac{1}{r^2}\frac{\partial}{\partial r}\left(r^2\frac{\partial T}{\partial r}\right) = \frac{1}{\alpha}\frac{\partial T}{\partial t}$$

$$\frac{d}{dr}\left(r^2\frac{dT}{dr}\right) = 0$$
 or $r\frac{d^2T}{dr^2} + 2\frac{dT}{dr} = 0$

Combined One-Dimensional Heat Conduction Equation

Overall, the one-dimensional transient heat conduction equations for the plane wall, cylinder, and sphere can be expressed as

$$\frac{1}{r^n}\frac{\partial}{\partial r}\left(r^n\,k\frac{\partial T}{\partial r}\right) + \dot{e}_{\rm gen} = \rho c\,\frac{\partial T}{\partial t}$$

n = 0 for a plane wall

- n = 1 for a cylinder
- n = 2 for a sphere

In the case of a plane wall, replace *r* by *x*.

This equation can be simplified for steady-state or no heat generation cases as described before.

GENERAL HEAT CONDUCTION EQUATION

Before, we considered one-dimensional heat conduction and assumed heat conduction in other directions to be negligible.

However, sometimes we need to consider heat transfer in other directions as well.

In such cases heat conduction is said to be *multidimensional,* and in this section we develop the governing differential equation in such systems in rectangular, cylindrical, and spherical.

Rectangular Coordinates

$$\begin{pmatrix} \text{Rate of heat} \\ \text{conduction at} \\ x, y, \text{ and } z \end{pmatrix} - \begin{pmatrix} \text{Rate of heat} \\ \text{conduction} \\ \text{at } x + \Delta x, \\ y + \Delta y, \text{ and } z + \Delta z \end{pmatrix} + \begin{pmatrix} \text{Rate of heat} \\ \text{generation} \\ \text{inside the} \\ \text{element} \end{pmatrix} = \begin{pmatrix} \text{Rate of change} \\ \text{of the energy} \\ \text{content of} \\ \text{the element} \end{pmatrix}$$

or

$$\dot{Q}_x + \dot{Q}_y + \dot{Q}_z - \dot{Q}_{x+\Delta x} - \dot{Q}_{y+\Delta y} - \dot{Q}_{z+\Delta z} + \dot{E}_{\text{gen, element}} = \frac{\Delta E_{\text{element}}}{\Delta t}$$
(2-36)

Noting that the volume of the element is $V_{\text{element}} = \Delta x \Delta y \Delta z$, the change in the energy content of the element and the rate of heat generation within the element can be expressed as

$$\Delta E_{\text{element}} = E_{t+\Delta t} - E_t = mc(T_{t+\Delta t} - T_t) = \rho c \Delta x \Delta y \Delta z (T_{t+\Delta t} - T_t)$$

$$\dot{E}_{\text{gen, element}} = \dot{e}_{\text{gen}} V_{\text{element}} = \dot{e}_{\text{gen}} \Delta x \Delta y \Delta z$$

Substituting into Eq. 2-36, we get

$$\dot{Q}_x + \dot{Q}_y + \dot{Q}_z - \dot{Q}_{x+\Delta x} - \dot{Q}_{y+\Delta y} - \dot{Q}_{z+\Delta z} + e_{\text{gen}} \Delta x \Delta y \Delta z = \rho c \Delta x \Delta y \Delta z \frac{T_{t+\Delta t} - T_t}{\Delta t}$$

Dividing by $\Delta x \Delta y \Delta z$ gives

$$-\frac{1}{\Delta y \Delta z} \frac{\dot{Q}_{x+\Delta x} - \dot{Q}_x}{\Delta x} - \frac{1}{\Delta x \Delta z} \frac{\dot{Q}_{y+\Delta y} - \dot{Q}_y}{\Delta y} - \frac{1}{\Delta x \Delta y} \frac{\dot{Q}_{z+\Delta z} - \dot{Q}_z}{\Delta z} + \dot{e}_{gen} =$$

$$\rho c \frac{T_{t+\Delta t} - T_t}{\Delta t} \tag{2-37}$$



FIGURE 2–20

Three-dimensional heat conduction through a rectangular volume element.

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Noting that the heat transfer areas of the element for heat conduction in the x, y, and z directions are $A_x = \Delta y \Delta z$, $A_y = \Delta x \Delta z$, and $A_z = \Delta x \Delta y$, respectively, and taking the limit as Δx , Δy , Δz and $\Delta t \rightarrow 0$ yields

$$\frac{\partial}{\partial x} \left(k \frac{\partial T}{\partial x} \right) + \frac{\partial}{\partial y} \left(k \frac{\partial T}{\partial y} \right) + \frac{\partial}{\partial z} \left(k \frac{\partial T}{\partial z} \right) + \dot{e}_{gen} = \rho c \frac{\partial T}{\partial t}$$
(2-38)

since, from the definition of the derivative and Fourier's law of heat conduction,

$$\lim_{\Delta x \to 0} \frac{1}{\Delta y \Delta z} \frac{\dot{Q}_{x + \Delta x} - \dot{Q}_x}{\Delta x} = \frac{1}{\Delta y \Delta z} \frac{\partial Q_x}{\partial x} = \frac{1}{\Delta y \Delta z} \frac{\partial}{\partial x} \left(-k \Delta y \Delta z \frac{\partial T}{\partial x} \right) = -\frac{\partial}{\partial x} \left(k \frac{\partial T}{\partial x} \right)$$
$$\lim_{\Delta y \to 0} \frac{1}{\Delta x \Delta z} \frac{\dot{Q}_{y + \Delta y} - \dot{Q}_y}{\Delta y} = \frac{1}{\Delta x \Delta z} \frac{\partial Q_y}{\partial y} = \frac{1}{\Delta x \Delta z} \frac{\partial}{\partial y} \left(-k \Delta x \Delta z \frac{\partial T}{\partial y} \right) = -\frac{\partial}{\partial y} \left(k \frac{\partial T}{\partial y} \right)$$
$$\lim_{\Delta z \to 0} \frac{1}{\Delta x \Delta y} \frac{\dot{Q}_{z + \Delta z} - \dot{Q}_z}{\Delta z} = \frac{1}{\Delta x \Delta y} \frac{\partial Q_z}{\partial z} = \frac{1}{\Delta x \Delta y} \frac{\partial}{\partial z} \left(-k \Delta x \Delta y \frac{\partial T}{\partial z} \right) = -\frac{\partial}{\partial z} \left(k \frac{\partial T}{\partial z} \right)$$

Eq. 2–38 is the general heat conduction equation in rectangular coordinates. In the case of constant thermal conductivity, it reduces to

$$\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} + \frac{\dot{e}_{gen}}{k} = \frac{1}{\alpha} \frac{\partial T}{\partial t}$$
(2-39)

where the property $\alpha = k/\rho c$ is again the *thermal diffusivity* of the material. Eq. 2–39 is known as the **Fourier-Biot equation**, and it reduces to these forms under specified conditions:

- (1) Steady-state:(called the **Poisson equation**)
- (2) *Transient, no heat generation:*(called the **diffusion equation**)
- (3) *Steady-state, no heat generation:* (called the **Laplace equation**)

$$\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} + \frac{\dot{e}_{gen}}{k} = 0$$
$$\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} = \frac{1}{\alpha} \frac{\partial T}{\partial t}$$
$$\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} = 0$$



The three-dimensional heat conduction equations reduce to the one-dimensional ones when the temperature varies in one dimension only.

Cylindrical Coordinates

Relations between the coordinates of a point in rectangular and cylindrical coordinate systems:

$$x = r \cos \phi$$
, $y = r \sin \phi$, and $z = z$

$$\frac{1}{r}\frac{\partial}{\partial r}\left(kr\frac{\partial T}{\partial r}\right) + \frac{1}{r^2}\frac{\partial T}{\partial \phi}\left(k\frac{\partial T}{\partial \phi}\right) + \frac{\partial}{\partial z}\left(k\frac{\partial T}{\partial z}\right) + \dot{e}_{gen} = \rho c \frac{\partial T}{\partial t}$$



Spherical Coordinates

Relations between the coordinates of a point in rectangular and spherical coordinate systems:

 $x = r \cos \phi \sin \theta$, $y = r \sin \phi \sin \theta$, and $z = \cos \theta$ $\frac{1}{r^2}\frac{\partial}{\partial r}\left(kr^2\frac{\partial T}{\partial r}\right) + \frac{1}{r^2\sin^2\theta}\frac{\partial}{\partial\phi}\left(k\frac{\partial T}{\partial\phi}\right) + \frac{1}{r^2\sin\theta}\frac{\partial}{\partial\theta}\left(k\sin\theta\frac{\partial T}{\partial\theta}\right) + \dot{e}_{\rm gen} = \rho c \frac{\partial T}{\partial t}$ $d\theta$ **v** dø x FIGURE 2–23 A differential volume element in 11 spherical coordinates.