



Antennas and Transmission Lines

Electrical Department-3rd Stage

By

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2025-2024

Linear Wire Antenna

Wire Antennas (Linear or Curved) are some of the oldest , simplest , cheapest , and in many cases the most versatile for many application.

❖ Infinitesimal Dipole (Hertz Antenna) ($L \ll \lambda$)

Short Dipole Current Element ($L \leq \lambda / 50$)

The current is assumed to be constant and given by:

$$\vec{I}(z) = I \vec{a}_z \quad (I = \text{constant})$$

Radiated fields it will be required to determine first $\vec{A}$ (magnetic vector potential) and then find $\vec{E}$ & $\vec{H}$ at P.

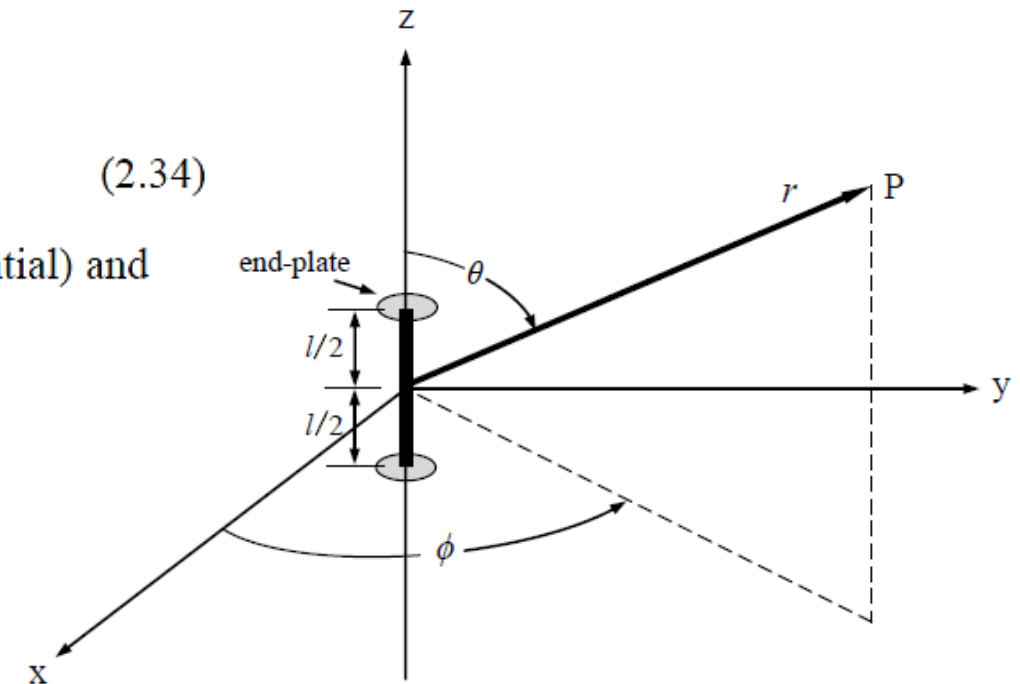
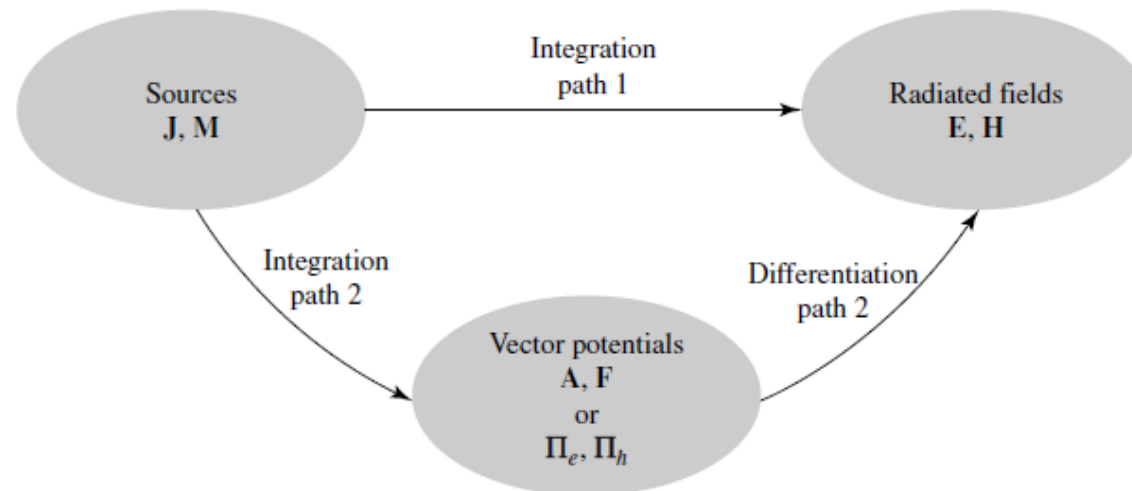


Figure 2.15 Infinitesimal dipole .

$$\vec{a}_r = \cos\theta \vec{a}_z + \sin\theta \sin\phi \vec{a}_y + \sin\theta \cos\phi \vec{a}_x$$

$\vec{A}$ is given by the following relation

$$\vec{A} = \frac{\mu}{2\pi} \int_v \frac{\vec{J}}{r} e^{-j\beta r} dv, \quad \vec{J} = \frac{I}{A}$$

$$dv = dx dy dz$$

$\mu = \text{Magnetic permeability}$

$J = \text{current density}$

$\beta = \text{propagation constant} = 2\pi/\lambda$

(2.36)

(2.37)

The current density $\vec{J}$ Integrated over the cross sectional area of wire (which is placed on xy plane) is $\vec{J}$ use current I.

$$\int dy dx \frac{I}{A} = I$$

(2.38)

$$\vec{A} = \frac{\mu}{4\pi} \int_{-\frac{\ell}{2}}^{\frac{\ell}{2}} \frac{\vec{I}}{r} e^{-j\beta r} dz$$

(2.39)

$$\vec{A} = \frac{\mu}{4\pi} \int_{-\frac{\ell}{2}}^{\frac{\ell}{2}} \frac{I_0}{r} e^{-j\beta r} dz \vec{a}_z$$

(2.40)

$$\vec{A} = \frac{\mu I_0 \ell e^{-j\beta r}}{4\pi r} \vec{a}_z, \quad A_x = A_y = 0$$

(2.41)

$$A_z = \frac{\mu I_0 \ell e^{-j\beta r}}{4\pi r}$$

(2.42)

$$\nabla \times \vec{A} = \vec{B}$$

(2.43)

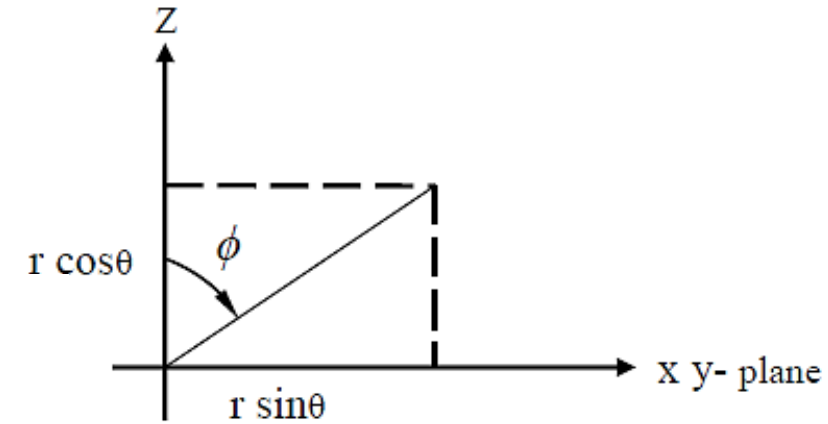


Figure 2.16 Coordinate system.

The transformation between rectangular and spherical components is given by:

$$\begin{bmatrix} A_r \\ A_\theta \\ A_\phi \end{bmatrix} = \begin{bmatrix} \sin\theta\cos\phi & \sin\theta\sin\phi & \cos\theta \\ \cos\theta\cos\phi & \cos\theta\sin\phi & -\sin\theta \\ -\sin\phi & \cos\phi & 0 \end{bmatrix} \begin{bmatrix} A_x \\ A_y \\ A_z \end{bmatrix} \quad (2.44)$$

$$A_r = A_z \cos\theta = \frac{\mu I_o \ell}{4\pi r} e^{-j\beta r} \cos\theta \quad (2.45)$$

$$A_\theta = -A_z \sin\theta = -\frac{\mu I_o \ell}{4\pi r} e^{-j\beta r} \sin\theta \quad (2.46)$$

$$A_\phi = 0 \quad (2.47)$$

$$\nabla \times \vec{A} = \vec{B} \quad (2.48)$$

$$\begin{aligned} \nabla \times \vec{A} = & \frac{1}{r \sin\theta} \left(\frac{\partial}{\partial \theta} (A_\phi \sin\theta) - \frac{\partial A_\theta}{\partial \phi} \right) \vec{a}_r + \frac{1}{r} \left(\frac{1}{\sin\theta} \frac{\partial A_r}{\partial \phi} - \frac{\partial}{\partial r} (r A_\phi) \right) \vec{a}_\theta \\ & + \frac{1}{r} \left(\frac{\partial}{\partial r} (r A_\theta) - \frac{\partial A_r}{\partial \theta} \right) \vec{a}_\phi \end{aligned} \quad (2.49)$$

$$\nabla \times \vec{A} = \frac{1}{r} \left(\frac{\partial}{\partial r} (r A_\theta) - \frac{\partial A_r}{\partial \theta} \right) \vec{a}_\phi \quad (2.50)$$

$$\vec{H} = \frac{j\beta I_o \ell}{4\pi r} \sin\theta \left(1 + \frac{1}{j\beta r} \right) e^{-j\beta r} \vec{a}_\phi \quad (2.51)$$

$$H_r = 0 \quad (2.52)$$

$$H_\theta = 0 \quad (2.53)$$

$$H_\phi = \frac{j\beta I_o \ell}{4\pi r} \sin\theta \left(1 + \frac{1}{j\beta r} \right) e^{-j\beta r} \quad (2.54)$$

in the same manner

$$\nabla \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t} \quad (2.55)$$

$$\vec{J} = \sigma \vec{E} \Rightarrow \vec{J} = 0 \quad \text{free space} \quad (2.56)$$

$$\nabla \times \vec{H} = j\omega\epsilon \vec{E} \quad (2.57)$$

$$\therefore E_r = \eta \frac{I_o \ell \cos\theta}{2\pi r^2} \left(1 + \frac{1}{j\beta r}\right) e^{-j\beta r} \quad (2.58)$$

$$\eta = 120\pi \quad (2.59)$$

$$E_\theta = j\eta \frac{\beta I_o \ell \sin\theta}{4\pi r} \left(1 + \frac{1}{j\beta r} - \frac{1}{(\beta r)^2}\right) e^{-j\beta r} \quad (2.60)$$

$$E_\phi = 0 \quad (2.61)$$

Near Field Region ($\beta r \ll 1$ or $r \ll \lambda$)

For $\beta r \ll 1$ ($r \ll \lambda$) the fields can be approximated by:

$$E_r = -j\eta \frac{I_o \ell e^{-j\beta r}}{2\pi \beta r^3} \cos\theta \quad (2.62)$$

$$E_\theta = -j\eta \frac{I_o \ell e^{-j\beta r}}{4\pi \beta r^3} \sin\theta \quad (2.63)$$

$$H_\phi = \frac{I_o \ell e^{-j\beta r}}{4\pi r^2} \sin\theta \quad (2.64)$$

$$E_\phi = H_r = H_\theta = 0 \quad (2.65)$$

Example For infinitesimal dipole (Near field region) prove that the average power density $\vec{W}_{av} = 0$.

The solution:- $\vec{W}_{av} = \frac{1}{2} \text{Re} [\vec{E} \otimes \vec{H}^*]$

$$\vec{W}_{av} = \frac{1}{2} \text{Re} \left[-j\eta \frac{I_o \ell e^{-j\beta r}}{2\pi\beta r^3} \cos\theta \vec{a}_r \otimes \frac{I_o \ell e^{-j\beta r}}{4\pi r^2} \sin\theta \vec{a}_\phi \right] = 0$$

$$\vec{W}_{av} = \frac{1}{2} \text{Re} \left[-j\eta \frac{I_o \ell e^{-j\beta r}}{4\pi\beta r^3} \sin\theta \vec{a}_\theta \otimes \frac{I_o \ell e^{-j\beta r}}{4\pi r^2} \sin\theta \vec{a}_\phi \right] = 0$$

Far Field Region $\beta r \gg 1$

$$E_\theta = j\eta \frac{\beta I_o \ell e^{-j\beta r}}{4\pi r} \sin\theta \quad (2.66)$$

$$H_\phi = j \frac{\beta I_o \ell e^{-j\beta r}}{4\pi r} \sin\theta \quad (2.67)$$

$$E_r = E_\phi = H_r = H_\theta = 0 \quad (2.68)$$

Parameters of infinitesimal dipole :

1- Radiation Resistance

$$\vec{W}_{av} = \frac{1}{2} \operatorname{Re} [\vec{E} \otimes \vec{H}^*]$$

$$\vec{W}_{av} = \frac{1}{2} \operatorname{Re} \left[j\eta \frac{\beta I_o \ell e^{-j\beta r}}{4\pi r} \sin\theta \vec{a}_\theta \otimes -j \frac{\beta I_o \ell e^{+j\beta r}}{4\pi r} \sin\theta \vec{a}_\phi \right]$$

$$\vec{W}_{av} = \frac{\eta}{2} \left[\frac{\beta I_o \ell}{4\pi r} \sin\theta \right]^2 \vec{a}_r$$

$$P_{rad} = \int \int \vec{W}_{av} \cdot \vec{ds}, \quad \vec{ds} = r^2 \sin\theta d\theta d\phi \vec{a}_r$$

$$P_{rad} = \int_0^{2\pi} \int_0^\pi \frac{\eta}{2} \left[\frac{\beta I_o \ell}{4\pi r} \right]^2 \sin^2\theta \vec{a}_r \cdot r^2 \sin\theta d\theta d\phi \vec{a}_r$$

$$P_{rad} = \frac{\eta}{2} \left[\frac{\beta I_o \ell}{4\pi} \right]^2 \int_0^{2\pi} \int_0^\pi \sin^3\theta d\theta d\phi$$

$$P_{rad} = \frac{\eta}{2} \beta^2 I_o^2 \left[\frac{I_o \ell}{4\pi} \right]^2 \left(\frac{4}{3} \right) (2\pi)$$

$$\text{where } I_o = \sqrt{2} I_{rms}, \beta = \frac{2\pi}{\lambda}, \eta = 120\pi$$

$$P_{rad} = \frac{120\pi}{2} \left(\frac{2\pi}{\lambda} \right)^2 (\sqrt{2} I_{rms})^2 \left[\frac{I_o \ell}{4\pi} \right]^2 \left(\frac{4}{3} \right) (2\pi)$$

$$P_{rad} = I_{rms}^2 \left(80\pi^2 \left(\frac{\ell}{\lambda} \right)^2 \right) \longleftrightarrow P_{rad} = I_{rms}^2 R_{rad}$$

$$R_{rad} = 80\pi^2 \left(\frac{\ell}{\lambda} \right)^2 \quad \text{only for } L \leq \frac{\lambda}{50}$$

2- Directivity

$$D_g(\theta, \phi) = 4\pi \frac{U(\theta, \phi)}{\iint U(\theta, \phi) d\Omega} = 4\pi \frac{\sin^2\theta}{\int_0^{2\pi} \int_0^\pi \sin^2\theta \sin\theta d\theta d\phi}$$

$$D_g(\theta, \phi) = 4\pi \frac{\sin^2\theta}{\int_0^{2\pi} \int_0^\pi \sin^3\theta d\theta d\phi} = 4\pi \frac{\sin^2\theta}{2\pi \left(\frac{4}{3}\right)}$$

$$D_0 = 4\pi \frac{(1)^2}{2\pi \left(\frac{4}{3}\right)}$$

$$D_0 = 1.5$$

3- HPBW

$$E(\theta, \phi) = j\eta \frac{\beta I_0 \ell e^{-j\beta r}}{4\pi r} \sin\theta$$

$$E(\theta, \phi)_n = \sin\theta$$

$$0.707(\max) = E(\theta, \phi)$$

$$0.707(1) = \sin\theta_h$$

$$\sin\theta_h = 0.707$$

$$\theta_h = \sin^{-1} 0.707 = 45^\circ$$

$$\text{HPBW} = 2(90 - \theta_h)$$

$$\text{HPBW} = 2(90^\circ - 45^\circ)$$

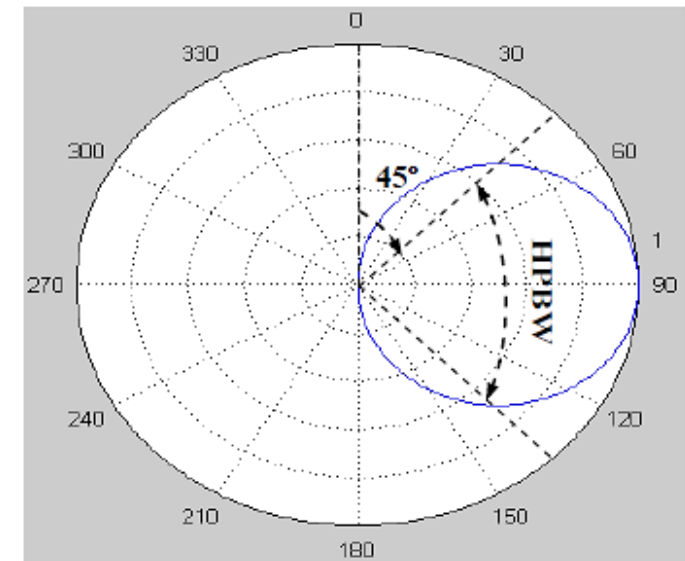
$$\text{HPBW} = 90^\circ$$

For Infinitesimal dipole $\left(L \leq \frac{\lambda}{50}\right)$

$$R_{rad} = 80\pi^2 \left(\frac{\ell}{\lambda}\right)^2$$

$$D_0 = 1.5$$

$$\text{HPBW} = 90^\circ$$



Example Derive an expression for the radiation resistance of a short dipole antenna.

The solution:- $\vec{W}_{av} = \frac{1}{2} R_e [\vec{E} \otimes \vec{H}^*]$

$$\vec{W}_{av} = \frac{1}{2} R_e \left[j\eta \frac{\beta I_o \ell e^{-j\beta r}}{4\pi r} \sin\theta \vec{a}_\theta \otimes -j \frac{\beta I_o \ell e^{+j\beta r}}{4\pi r} \sin\theta \vec{a}_\phi \right]$$

$$\vec{W}_{av} = \frac{\eta}{2} \left[\frac{\beta I_o \ell}{4\pi r} \sin\theta \right]^2 \vec{a}_r$$

$$P_{rad} = \int \int \vec{W}_{av} \cdot \vec{ds}, \quad \vec{ds} = r^2 \sin\theta d\theta d\phi \vec{a}_r$$

$$P_{rad} = \int_0^{2\pi} \int_0^\pi \frac{\eta}{2} \left[\frac{\beta I_o \ell}{4\pi r} \right]^2 \sin^2\theta \vec{a}_r \cdot r^2 \sin\theta d\theta d\phi \vec{a}_r$$

$$P_{rad} = \frac{\eta}{2} \left[\frac{\beta I_o \ell}{4\pi} \right]^2 \int_0^{2\pi} \int_0^\pi \sin^3\theta d\theta d\phi$$

$$P_{rad} = \frac{\eta}{2} \beta^2 I_o^2 \left[\frac{I_o \ell}{4\pi} \right]^2 \left(\frac{4}{3} \right) (2\pi) \quad \text{where } I_o = \sqrt{2} I_{rms}, \beta = \frac{2\pi}{\lambda}, \eta = 120\pi$$

$$P_{rad} = \frac{120\pi}{2} \left(\frac{2\pi}{\lambda} \right)^2 (\sqrt{2} I_{rms})^2 \left[\frac{I_o \ell}{4\pi} \right]^2 \left(\frac{4}{3} \right) (2\pi)$$

$$P_{rad} = I_{rms}^2 \left(80\pi^2 \left(\frac{\ell}{\lambda} \right)^2 \right) \longleftrightarrow P_{rad} = I_{rms}^2 R_{rad}$$

$$R_{rad} = 80\pi^2 \left(\frac{\ell}{\lambda} \right)^2$$

❖ Finite Length Dipole ($L > \lambda/10$)

Assume sinusoidal current distribution

$$I = I_m \sin \beta \left(\frac{L}{2} - z \right) \quad z > 0$$

$$I = I_m \sin \beta \left(\frac{L}{2} + z \right) \quad z < 0$$

The current is zero at the ends of the dipole since the current in the $\vec{a}_z$ -direction. The magnetic potential vector $\vec{A}$ is also in the z -direction.

$$A_z = \frac{\mu}{4\pi} \int_{-H}^H \frac{I e^{-j\beta R}}{R} dz \quad \begin{array}{l} \longrightarrow R = (r - z \cos \theta) \text{ for phase} \\ \longrightarrow R = r \text{ for amplitude} \end{array}$$

$$A_z = \frac{\mu}{4\pi r} \int_{-H}^0 I_m \sin \beta (H + z) e^{-j\beta (r - z \cos \theta)} dz + \frac{\mu}{4\pi r} \int_0^H I_m \sin \beta (H - z) e^{-j\beta (r - z \cos \theta)} dz \quad (2.73)$$

where L : dipole length

H : Half dipole length

$$\frac{L}{2} = H \quad (2.74)$$

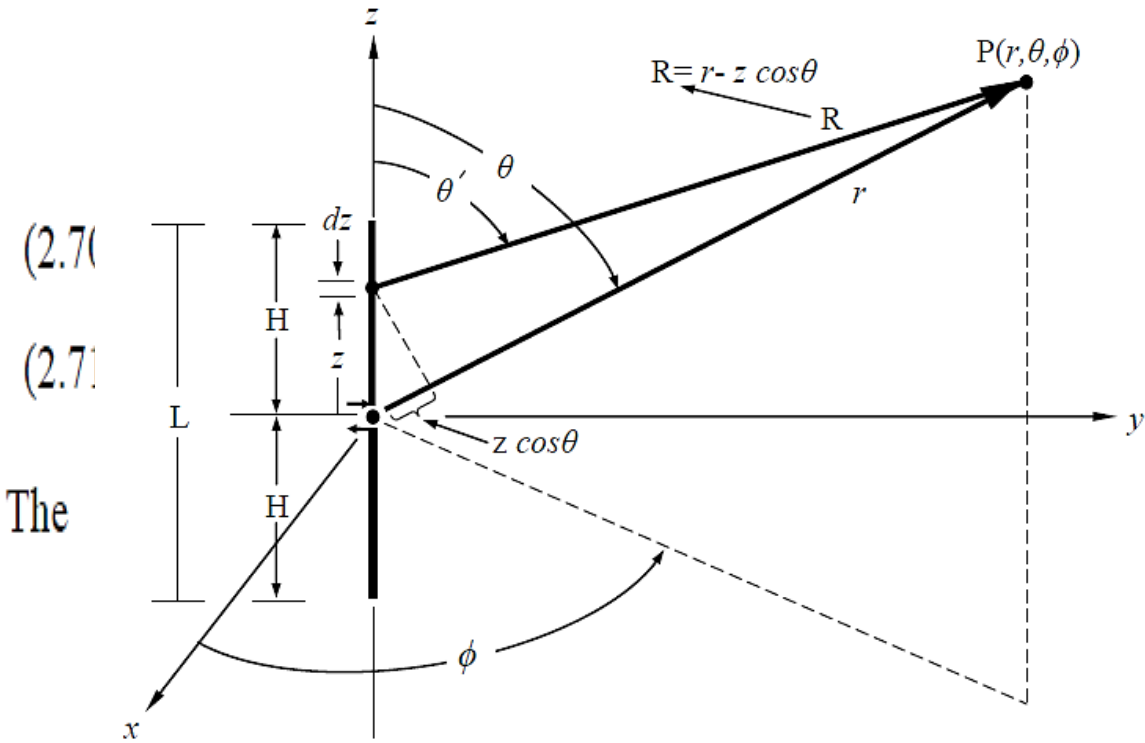


Figure 2.18 Finite Length dipole .

The general expression for the distance electric field of a dipole antenna ($L > \frac{\lambda}{10}$) is given by:

$$E_{\theta} = \frac{j60I_m e^{-j\beta r}}{r} \left[\frac{\cos\left(\frac{\beta L}{2} \cos\theta\right) - \cos\left(\frac{\beta L}{2}\right)}{\sin\theta} \right]$$

1- ($\lambda/2$) Dipole

One of the most commonly used antennas is the half-wavelength ($l = \lambda/2$) dipole. Because its radiation resistance is 73 ohms, which is very near the 50-ohm or 75-ohm characteristic impedances of some transmission lines, its matching to the line is simplified especially at resonance. Because of its wide acceptance in practice, we will examine in a little more detail its radiation

$$\frac{\beta L}{2} \cos \theta = \frac{2\pi \lambda}{2\lambda} \cos \theta = \frac{\pi}{2} \cos \theta \quad , \quad \cos\left(\frac{\beta L}{2}\right) = \cos\left(\frac{2\pi \lambda}{2\lambda}\right) = \cos\left(\frac{\pi}{2}\right) = 0$$

$$\vec{E} = \frac{j60I_m e^{-j\beta r}}{r} \left[\frac{\cos\left(\frac{\pi}{2} \cos \theta\right)}{\sin \theta} \right] \vec{a}_\theta \quad , \quad H_\phi = \frac{E_\theta}{\eta}$$

$$\vec{W}_{av} = \frac{1}{2} R_e \left[\vec{E} \otimes \vec{H}^* \right]$$

$$\vec{W}_{av} = \frac{1}{2} R_e \left[\frac{j60I_m e^{-j\beta r}}{r} \left[\frac{\cos\left(\frac{\pi}{2} \cos \theta\right)}{\sin \theta} \right] \vec{a}_\theta \otimes \frac{-j60I_m e^{j\beta r}}{\eta r} \left[\frac{\cos\left(\frac{\pi}{2} \cos \theta\right)}{\sin \theta} \right] \vec{a}_\phi \right]$$

$$\vec{W}_{av} = \frac{1}{2\eta} \left(\frac{60I_m}{r} \right)^2 \left[\frac{\cos\left(\frac{\pi}{2} \cos \theta\right)}{\sin \theta} \right]^2 \vec{a}_r$$

$$P_{rad} = \int \int \vec{W}_{av} \cdot \vec{ds} \quad , \quad \vec{ds} = r^2 \sin \theta \, d\theta \, d\phi \, \vec{a}_r$$

$$P_{rad} = \int_0^{2\pi} \int_0^\pi \frac{1}{2\eta} \left(\frac{60I_m}{r} \right)^2 \left[\frac{\cos\left(\frac{\pi}{2} \cos \theta\right)}{\sin \theta} \right]^2 \vec{a}_r \, r^2 \sin \theta \, d\theta \, d\phi \, \vec{a}_r$$

$$P_{rad} = \frac{1}{2\eta} (60I_m)^2 (2\pi) \int_0^\pi \frac{\cos^2\left(\frac{\pi}{2} \cos \theta\right)}{\sin \theta} \, d\theta$$

$$P_{rad} = 60I_{rms}^2 \int_0^\pi \frac{\cos^2\left(\frac{\pi}{2} \cos \theta\right)}{\sin \theta} \, d\theta \quad , \quad \int_0^\pi \frac{\cos^2\left(\frac{\pi}{2} \cos \theta\right)}{\sin \theta} \, d\theta = 1.218$$

$$P_{rad} = 73 I_{rms}^2 \Rightarrow R_{rad} = 73 \, \Omega$$

These equations are used to determine Prad, Wav, Rr for $(\lambda/2)$ Dipole

Directivity

$$D = 4\pi \frac{U(\theta, \phi)|_{max}}{\iint U(\theta, \phi) d\Omega} = 4\pi \frac{|E_{\theta max}|^2}{\int_0^{2\pi} \int_0^{\pi} |E_{\theta}|^2 \sin\theta d\theta d\phi}$$

$$D = 4\pi \frac{\left| \frac{\cos(\frac{\pi}{2}\cos\theta)}{\sin\theta} \right|^2}{2\pi \int_0^{\pi} \left| \frac{\cos(\frac{\pi}{2}\cos\theta)}{\sin\theta} \right|^2 \sin\theta d\theta} = 4\pi \frac{(1)^2}{2\pi \int_0^{\pi} \left| \frac{\cos(\frac{\pi}{2}\cos\theta)}{\sin\theta} \right|^2 \sin\theta d\theta}$$

$$D = 4\pi \frac{1}{2\pi(1.218)} = 1.64$$

HPBW

$$E(\theta, \phi) = \frac{\cos\left(\frac{\pi}{2}\cos\theta\right)}{\sin\theta}$$

$$0.707(max) = E(\theta, \phi)$$

$$0.707(1) = \frac{\cos\left(\frac{\pi}{2}\cos\theta\right)}{\sin\theta}$$

$$0.707\sin\theta_h = \cos\left(\frac{\pi}{2}\cos\theta\right)$$

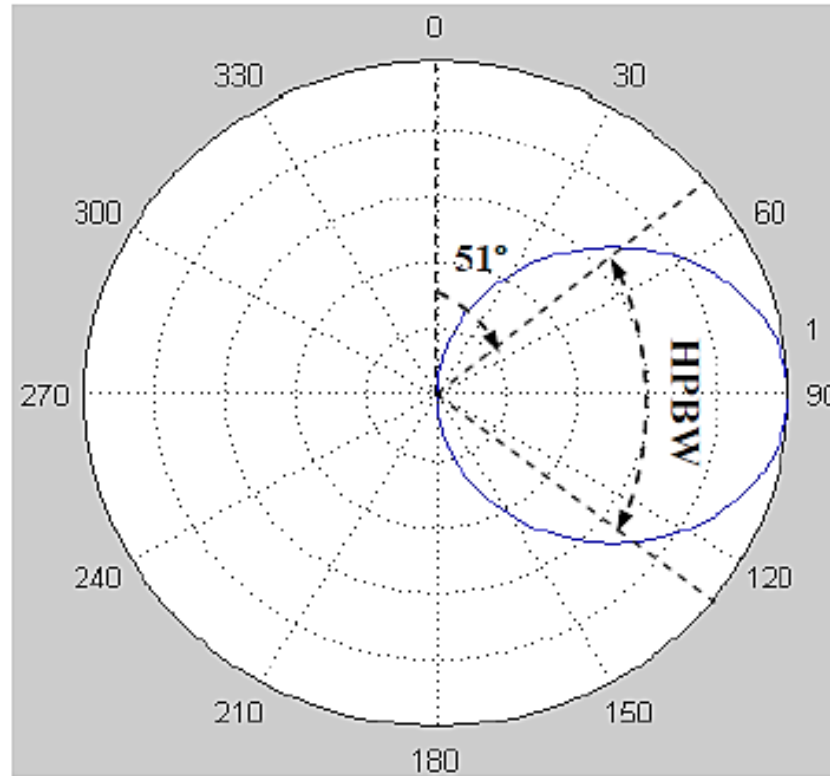
$$\theta_h = \sin^{-1}\left[\sqrt{2}\cos\left(\frac{\pi}{2}\cos\theta\right)\right]$$

$$\theta_h = 51^\circ$$

$$\text{HPBW} = 2(90 - \theta_h)$$

$$\text{HPBW} = 2(90^\circ - 51^\circ)$$

$$\text{HPBW} = 78^\circ$$



θ	$E(\theta, \phi)$
0	0
30°	0.417
45°	0.627
60°	0.816
90°	1

Figure 2.19 Radiation pattern of the antenna .

2- $\lambda/4$ dipole

These equations are used to determine P_{rad} , W_{av} , R_r for $(\lambda/4)$ Dipole

$$\frac{\beta L}{2} \cos \theta = \frac{2\pi \lambda}{2\lambda} \frac{1}{4} \cos \theta = \frac{\pi}{4} \cos \theta \quad , \quad \cos\left(\frac{\beta L}{2}\right) = \cos\left(\frac{2\pi \lambda}{2\lambda} \frac{1}{4}\right) = \cos\left(\frac{\pi}{4}\right) = 0.707$$

$$\vec{E} = \frac{j60I_m e^{-j\beta r}}{r} \left[\frac{\cos\left(\frac{\pi}{4} \cos \theta\right) - 0.707}{\sin \theta} \right] \vec{a}_\theta \quad , \quad H_\phi = \frac{E_\theta}{\eta}$$

$$\vec{W}_{av} = \frac{1}{2} R_e \left[\vec{E} \otimes \vec{H}^* \right]$$

$$\vec{W}_{av} = \frac{1}{2} R_e \left[\frac{j60I_m e^{-j\beta r}}{r} \left[\frac{\cos\left(\frac{\pi}{4} \cos \theta\right) - 0.707}{\sin \theta} \right] \vec{a}_\theta \otimes \frac{-j60I_m e^{j\beta r}}{\eta r} \left[\frac{\cos\left(\frac{\pi}{4} \cos \theta\right) - 0.707}{\sin \theta} \right] \vec{a}_\phi \right]$$

$$\vec{W}_{av} = \frac{1}{2\eta} \left(\frac{60I_m}{r} \right)^2 \left[\frac{\cos\left(\frac{\pi}{4} \cos \theta\right) - 0.707}{\sin \theta} \right]^2 \vec{a}_r$$

$$P_{rad} = \int \int \vec{W}_{av} \cdot \vec{ds} \quad , \quad \vec{ds} = r^2 \sin \theta \, d\theta \, d\phi \, \vec{a}_r$$

$$P_{rad} = \int_0^{2\pi} \int_0^\pi \frac{1}{2\eta} \left(\frac{60I_m}{r} \right)^2 \left[\frac{\cos\left(\frac{\pi}{4} \cos \theta\right) - 0.707}{\sin \theta} \right]^2 \vec{a}_r \, r^2 \sin \theta \, d\theta \, d\phi \, \vec{a}_r$$

$$P_{rad} = \frac{1}{2\eta} (60I_m)^2 (2\pi) \int_0^\pi \frac{[\cos\left(\frac{\pi}{4} \cos \theta\right) - 0.707]^2}{\sin \theta} \, d\theta$$

$$P_{rad} = 60I_{rms}^2 \int_0^\pi \frac{[\cos\left(\frac{\pi}{4} \cos \theta\right) - 0.707]^2}{\sin \theta} \, d\theta \quad , \quad \int_0^\pi \frac{[\cos\left(\frac{\pi}{4} \cos \theta\right) - 0.707]^2}{\sin \theta} \, d\theta = 0.114$$

$$P_{rad} = 6.84 I_{rms}^2 \Rightarrow R_{rad} = 6.84 \, \Omega$$

Directivity

$$D = 4\pi \frac{U(\theta, \phi)|_{\max}}{\iint U(\theta, \phi) d\Omega} = 4\pi \frac{|E_{\theta\max}|^2}{\int_0^{2\pi} \int_0^\pi |E_\theta|^2 \sin\theta d\theta d\phi}$$

θ	$ E(\theta, \phi) $
0	0
30°	0.14
45°	0.2018
60°	0.25
90°	0.293

$$D = 4\pi \frac{\left| \frac{\cos(\frac{\pi}{4}\cos\theta) - 0.707}{\sin\theta} \right|^2}{2\pi \int_0^\pi \frac{\cos(\frac{\pi}{4}\cos\theta) - 0.707}{\sin\theta}^2 \sin\theta d\theta}$$

$$D = 4\pi \frac{(0.293)^2}{2\pi \int_0^\pi \left| \frac{\cos(\frac{\pi}{4}\cos\theta) - 0.707}{\sin\theta} \right|^2 \sin\theta d\theta} = 4\pi \frac{(0.293)^2}{2\pi \int_0^\pi \frac{[\cos(\frac{\pi}{4}\cos\theta) - 0.707]^2}{\sin^2\theta} \sin\theta d\theta}$$

$$D = 4\pi \frac{(0.293)^2}{2\pi \int_0^\pi \frac{[\cos(\frac{\pi}{4}\cos\theta) - 0.707]^2}{\sin\theta} d\theta}$$

$$D = 4\pi \frac{(0.293)^2}{2\pi(0.114)}$$

$$D = 1.506$$

HPBW

$$E(\theta, \phi) = \frac{\cos(\frac{\pi}{4}\cos\theta) - 0.707}{\sin\theta}$$

$$0.707(max) = E(\theta, \phi)$$

$$0.707(0.293) = \frac{\cos(\frac{\pi}{4}\cos\theta) - 0.707}{\sin\theta}$$

$$0.207\sin\theta_h = \cos\left(\frac{\pi}{4}\cos\theta\right) - 0.707$$

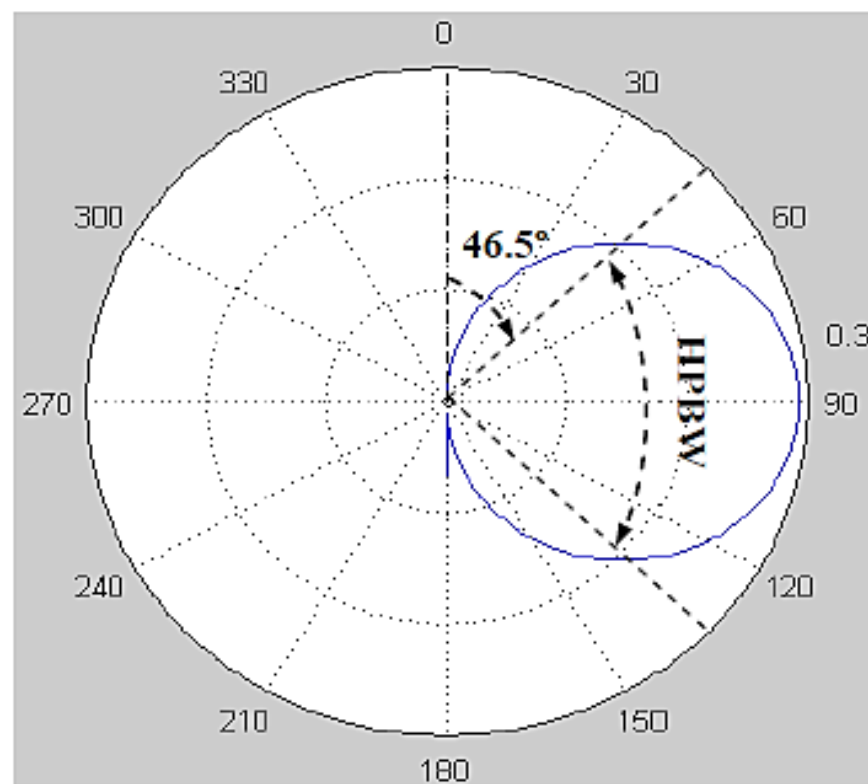
$$\theta_h = \sin^{-1} \frac{1}{0.207} \left[\cos\left(\frac{\pi}{4}\cos\theta\right) - 0.707 \right]$$

$$\theta_h = 46.5^\circ$$

$$\text{HPBW} = 2(90 - \theta_h)$$

$$\text{HPBW} = 2(90^\circ - 46.5^\circ)$$

$$\text{HPBW} = 87^\circ$$



θ	$ E(\theta, \phi) $
0	0
30°	0.14
45°	0.2018
60°	0.25
90°	0.293

Figure 2.20 Radiation pattern of the antenna .

Thank You